



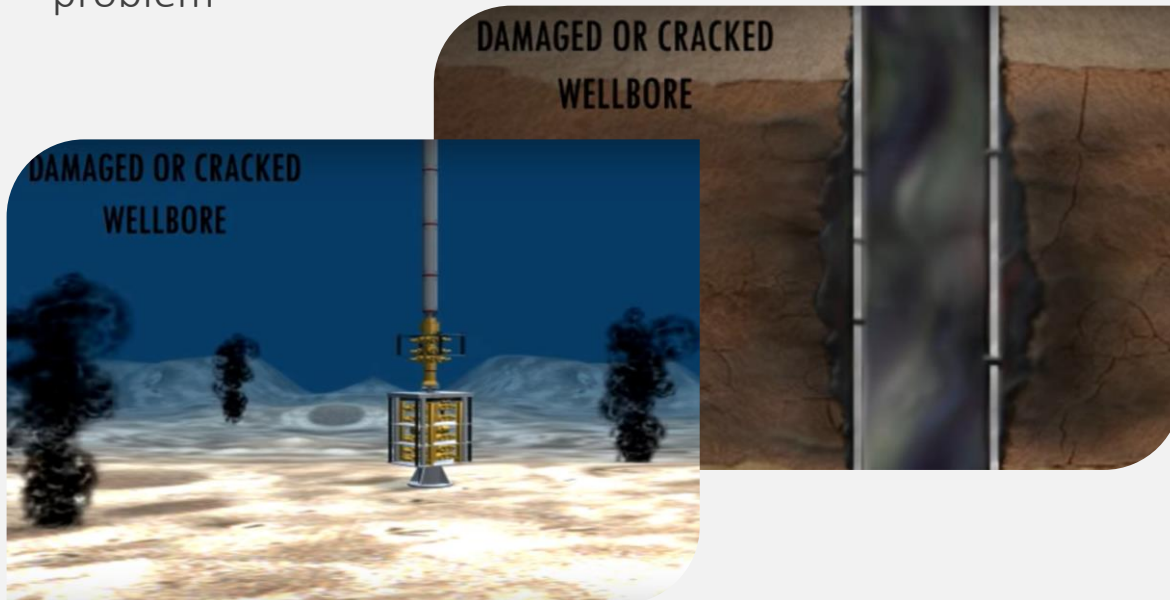
Preventing oil spills:

How spintronics will change the game

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Quick facts on oil-related accidents

- ❖ In the United States, from 1971 through 2000, the Coast Guard recorded over **250,000** oil spills in U.S. Waters.
- ❖ The largest oil spill in US history (2010, Gulf of Mexico), brought about: **200 millions** gallons of oil spilt, **\$56 billion** of fines and costs, **11** people dead, **17** injured, **thousands** of animals dead.
- ❖ Among the causes of the catastrophe, experts name **concrete integrity issues** and **late identification** of the problem



KAUST proposal

Parameters of the model:

- Desired frequency range of 1-10 kHz
- Temperature in the wellbore goes up to 100 °C, heat insulation will be required to protect the electronics
- Original paper assumes a large transmitter coil and high relative permeability of concrete (up to 2)
- Design is not suitable for MTJ's use: signal will be too small, we plan to use a gradiometer instead

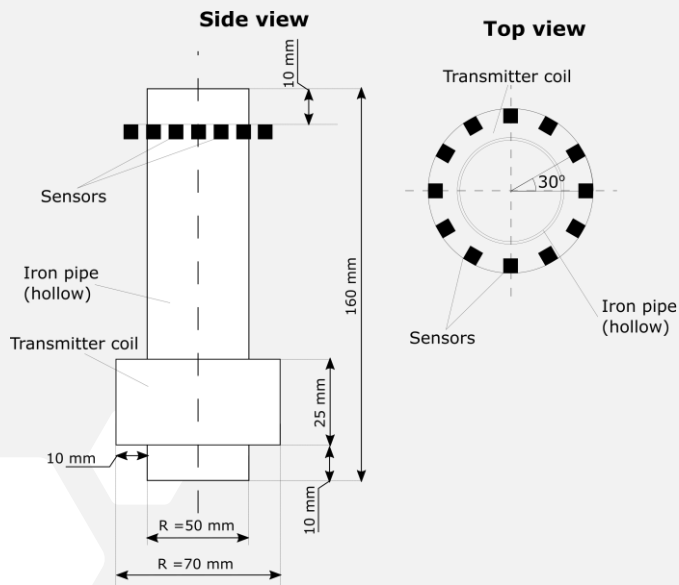


Fig. 2. The original design (by Timofey Eltsov)

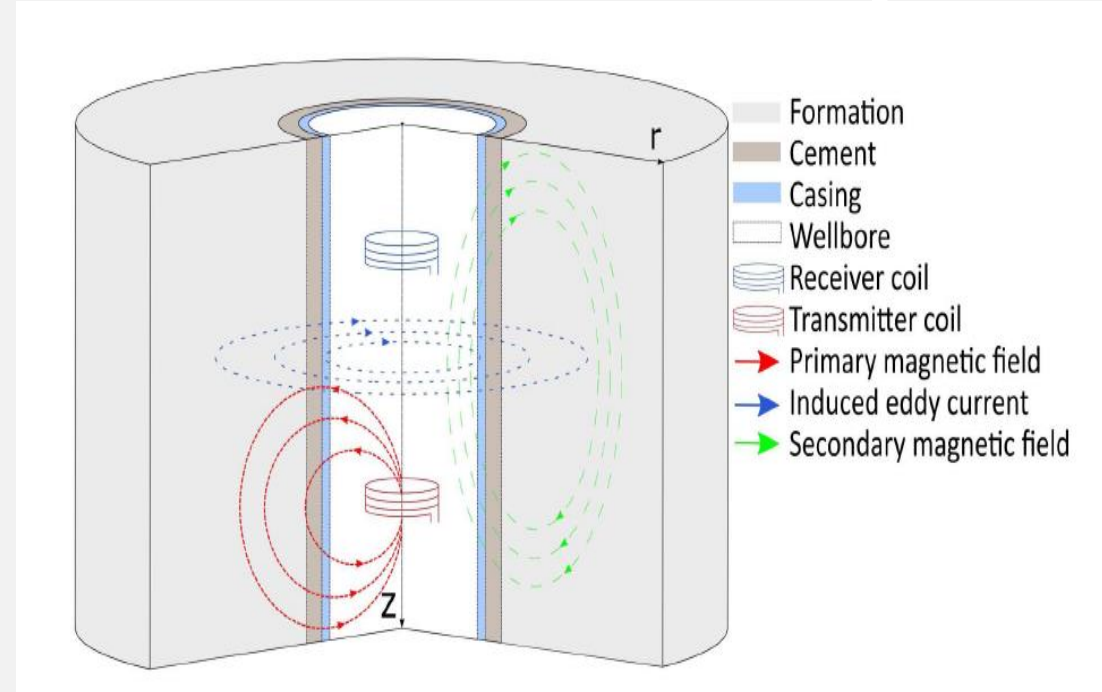


Fig. 1. A model of wellbore (by Timofey Eltsov)

Parameter	Wellbore	Fiberglass	Concrete	Formation
Radius, m	0.07	0.1	0.15	
Resistivity, $\Omega \cdot m$	2	10^8	100	50
Magnetic permeability	1	1	1 - 2	1

MTJ – Magnetic Tunnel Junction

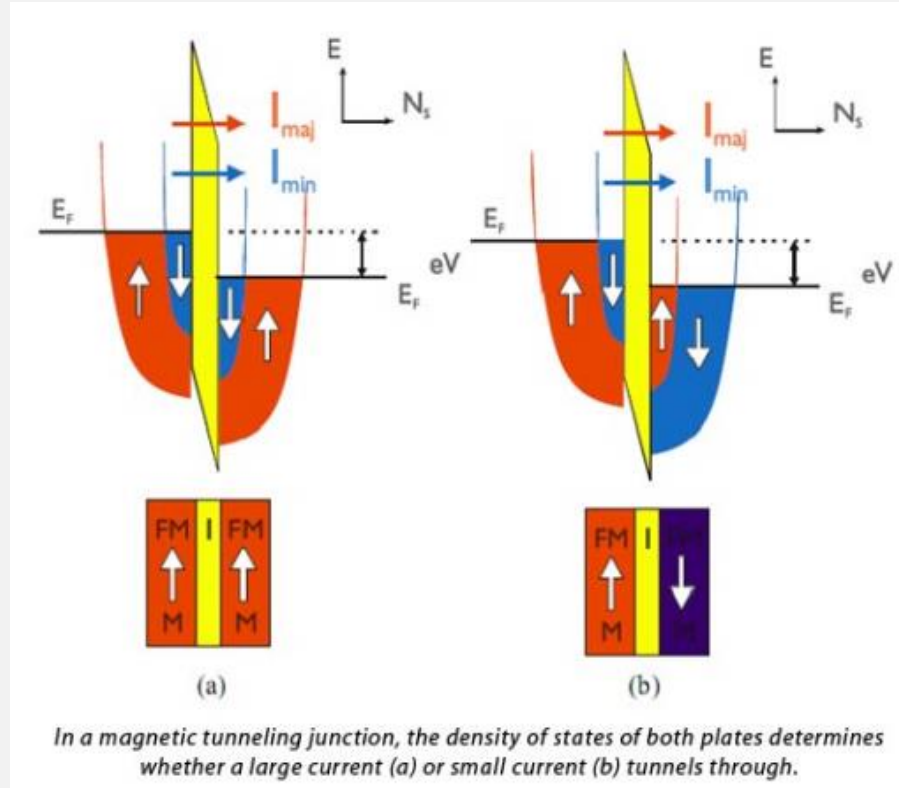


Fig. 3. Spin-dependent tunneling

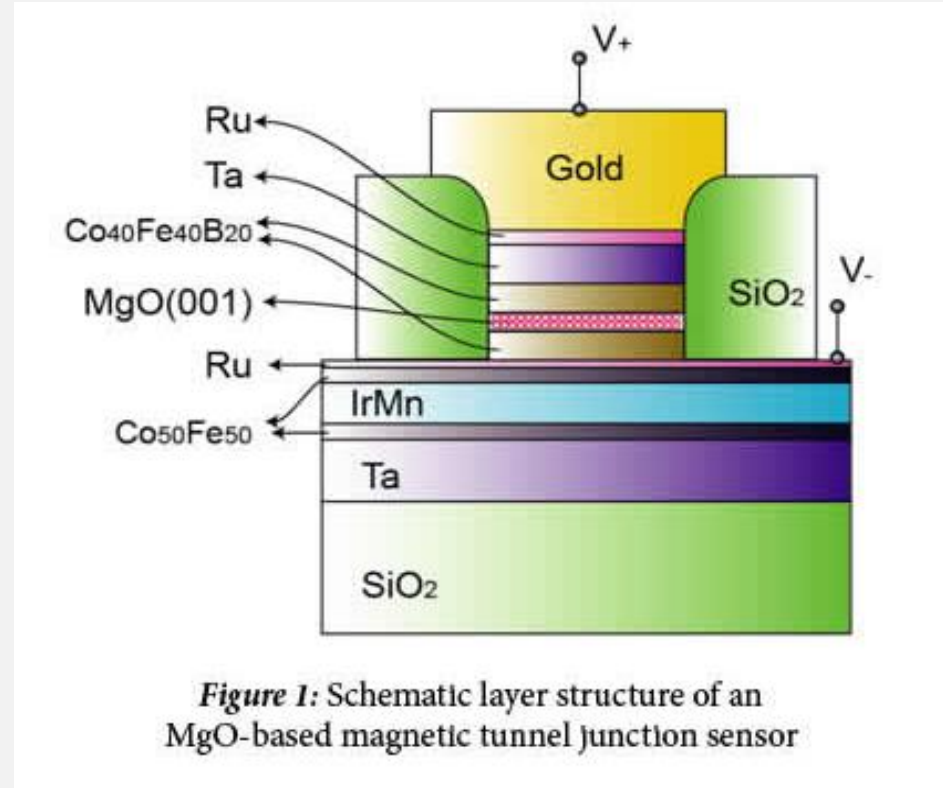


Figure 1: Schematic layer structure of an MgO-based magnetic tunnel junction sensor

Fig. 4. A typical MTJ structure



**Part I:
Simulation**

2D simulation (COMSOL)

Geometrical sizes were preserved from the original proposal

Materials: granite, concrete (relative magnetic permeability 1.02), fiberglass, oil (to replace drilling mud), air

Distance from the probes to the fiberglass: 1 cm

Field source: magnetic point dipole $0.01 \text{ A}\cdot\text{m}^2$

DC mode used to save time

2 configurations tested, parallel and perpendicular to the surface (parametric sweep of the position of the cavity)

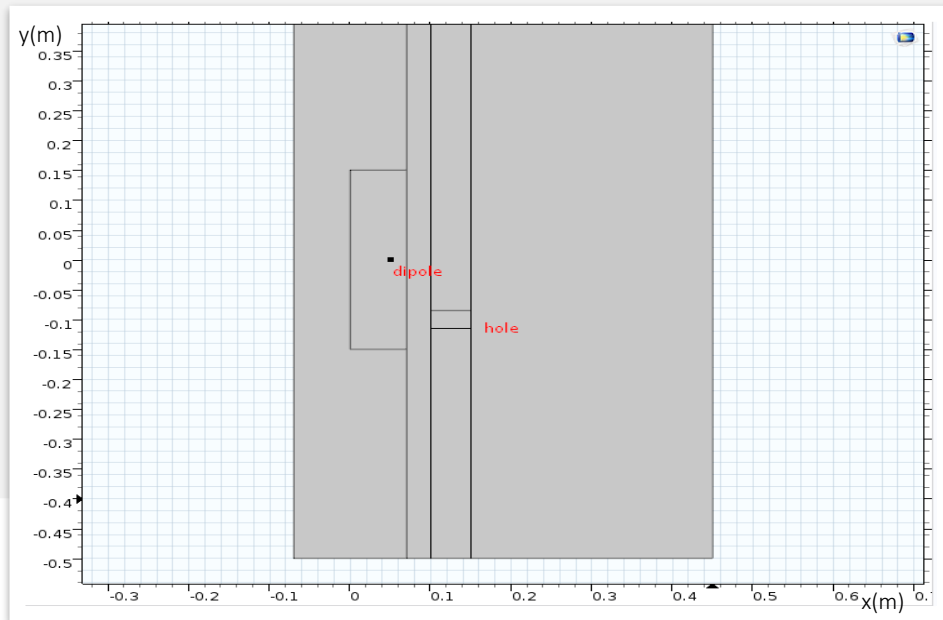


Fig. 5. The 2D model of a wellbore

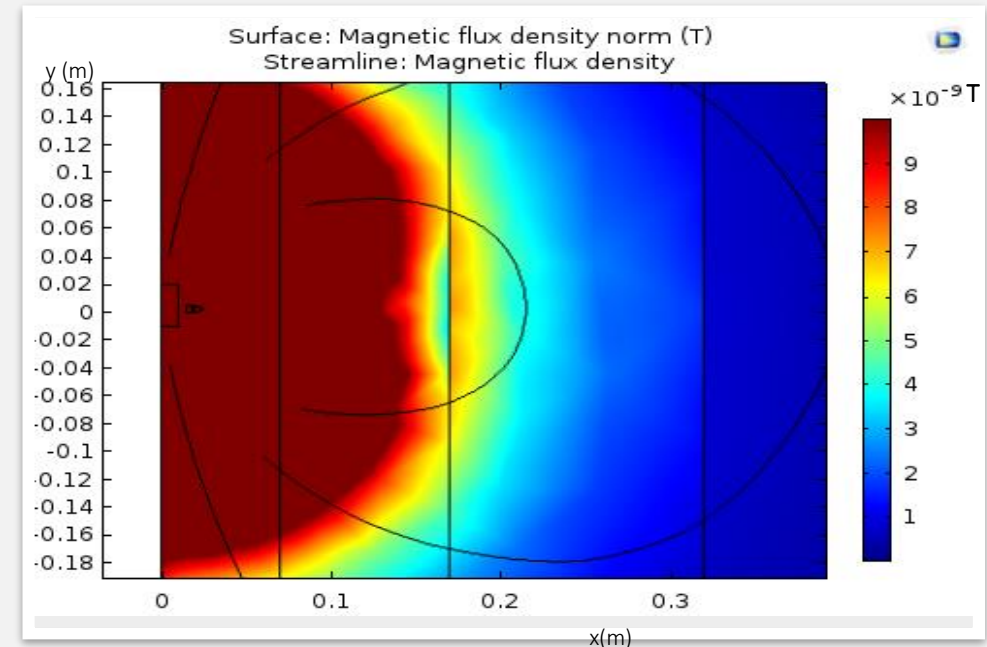


Fig. 6. Simulated magnetic response of the concrete

Signal (2D results)

- pT range of the signal – can be resolved by using stronger coil field
- Simulation results demonstrate a constant offset of the signal (removed here), 2-3 orders of magnitude greater than the signal itself

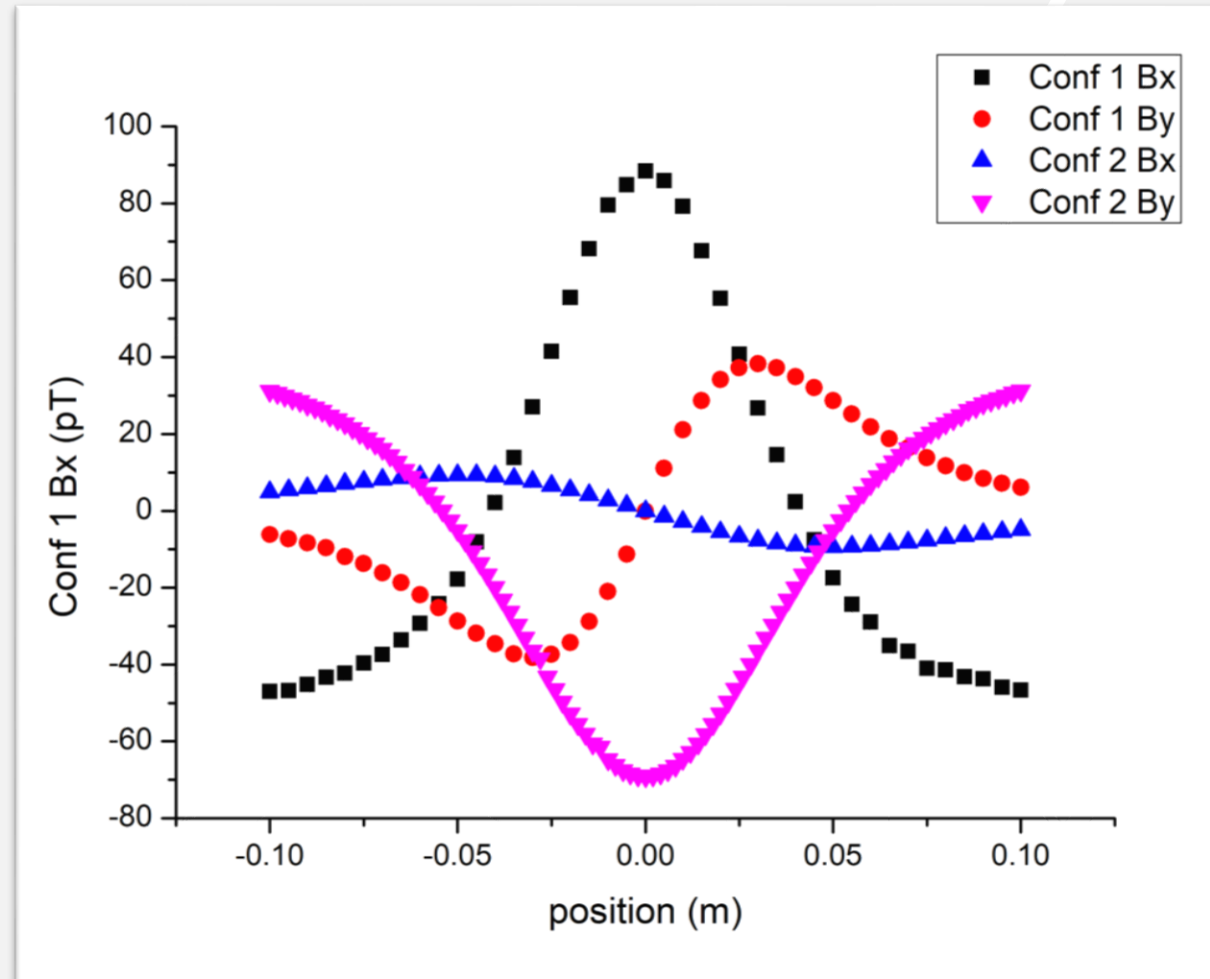
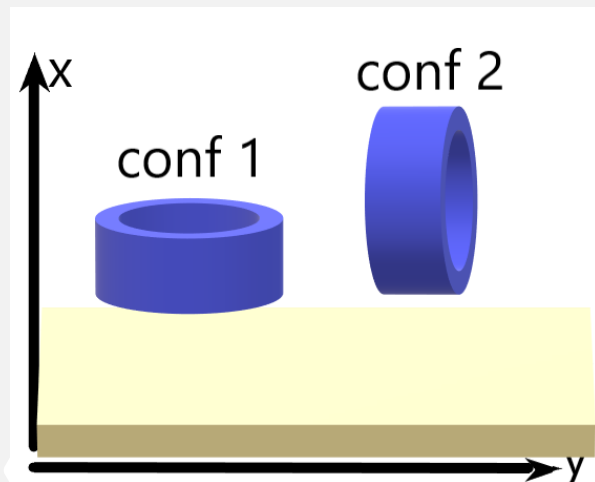


Fig. 7. The predicted gradiometer signal (adjusted)



Part II: Experiment

Magnetic sand

Limitations and issues:

- Non-uniform mixing – sand grain size varies and a light shaking of the box will cause iron powder to slide downwards – switched to using gypsum powder instead of sand to build a solid piece of “concrete”
- Desired upper limit on the iron amount – 3 % by mass
- Steel powder magnetization turned out to be weaker than that for the bulk iron

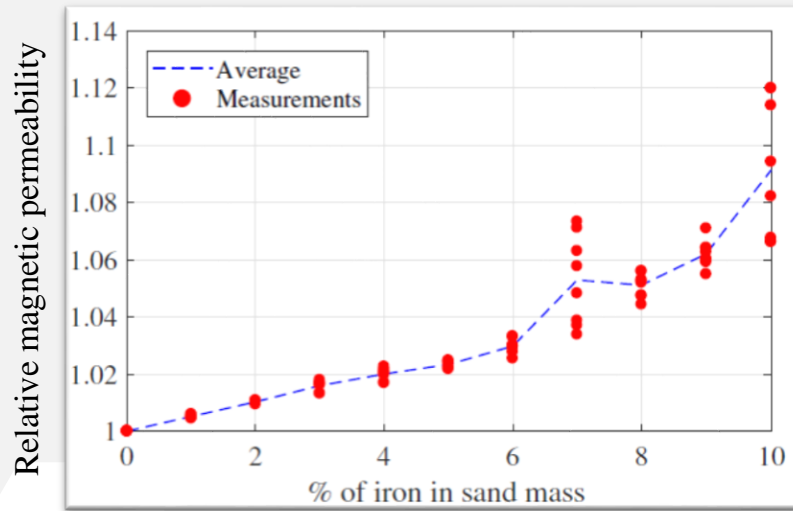


Fig. 8. Measured relative permeability of concrete (performed by KAUST group)

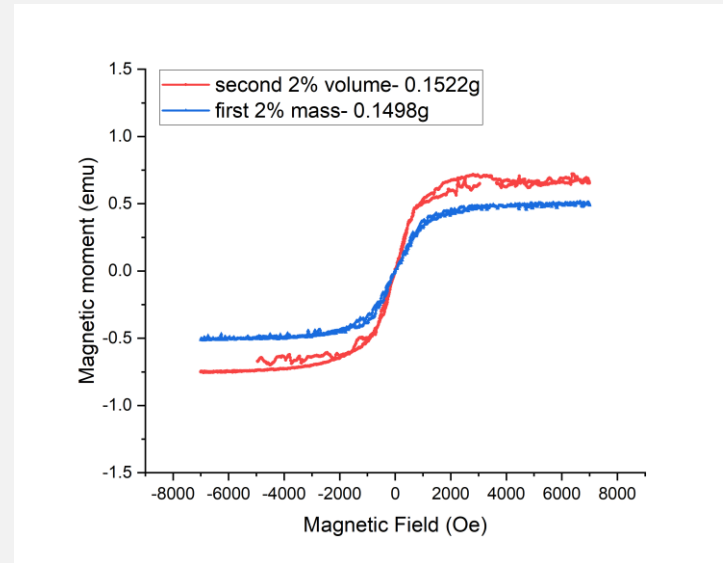


Fig. 9. Measured magnetizations of mixtures

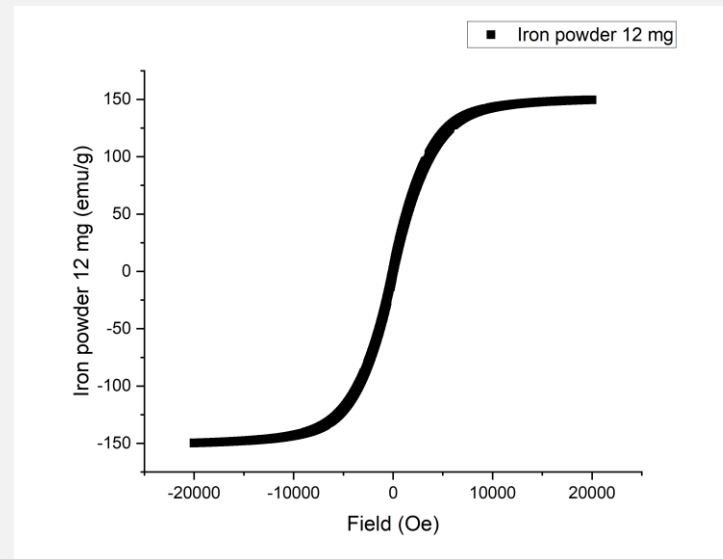


Fig. 10. Measured magnetization of iron powder



Density of sand: $1,75 \text{ g/cm}^3$
 Density of iron powder: $3,59 \text{ g/cm}^3$

Saturation magnetization measurements results:

2% mass measurement:

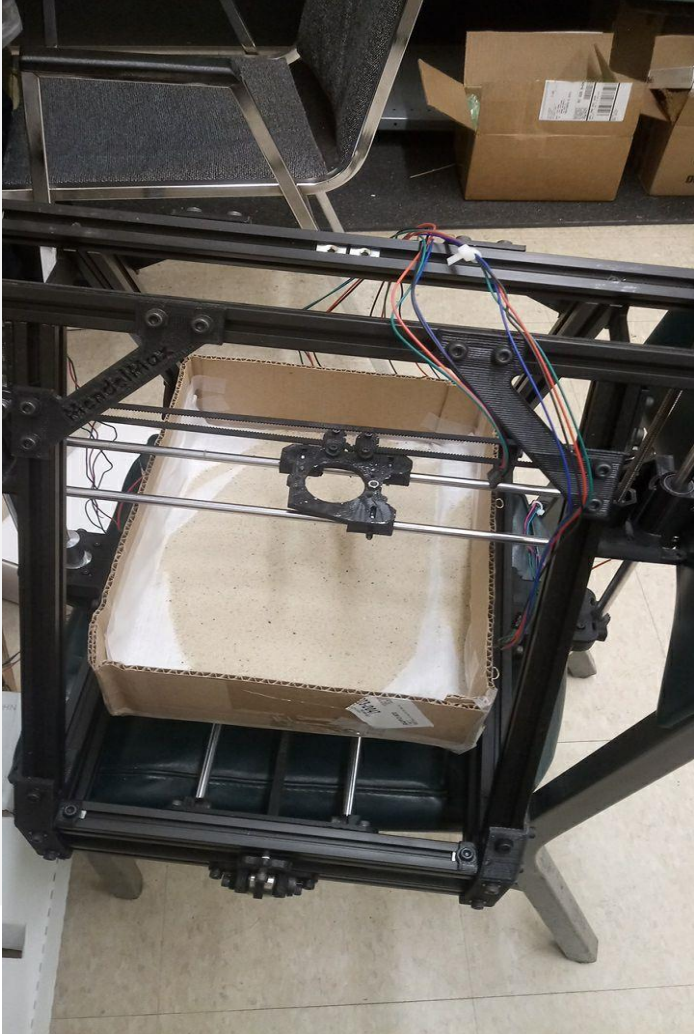
- Predicted: 0.44 emu
- Measured: 0.5 emu (+13% error)

2% volume measurement (porosity effects not included)

- Predicted: 0.9 emu
- Measured: 0,7 emu (-23% error)

- Non-uniform mixing
- Cavities contributions

Examples of the issues with concrete modelling



Helmholtz coil calibration

- Satisfactory but not ideal field of the coil itself
- Uniform field is not truly uniform and sensor can easily detect it -> cannot minimize CMR ratio well

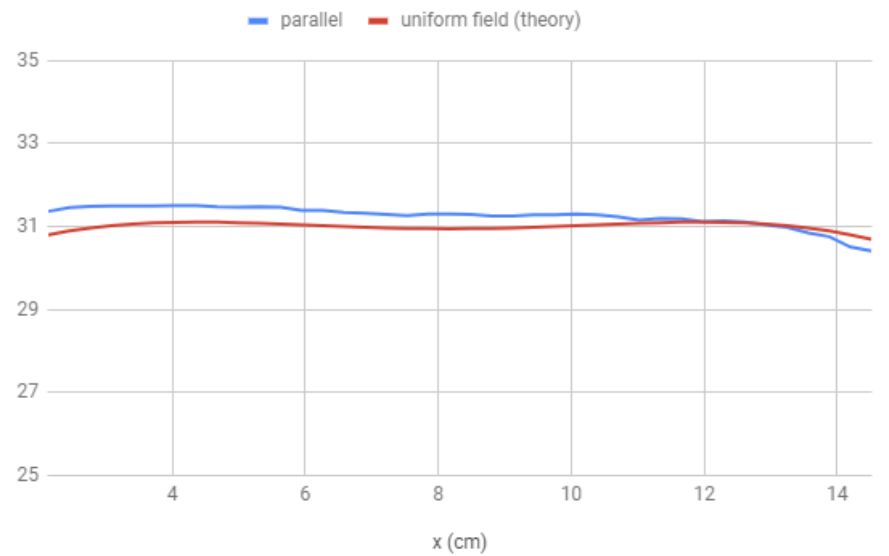
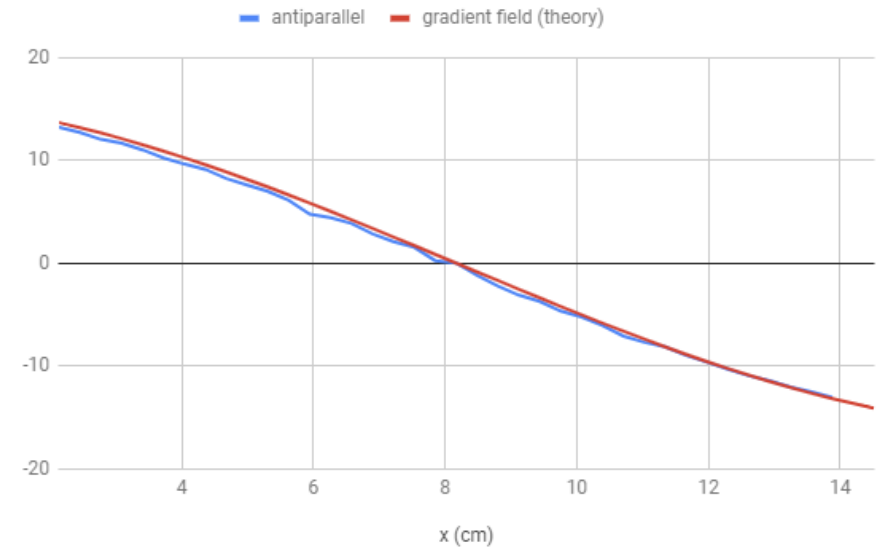


Fig. 11. Helmholtz coil calibration

Sensor calibration

- Inconsistent
- The output might be dependent on the field to some extent
- Uniform-field fit seems to be more consistent
- Unexplained dip in the middle of gradient field curve
- Saturation field of MTJ limits the use of the coil potential

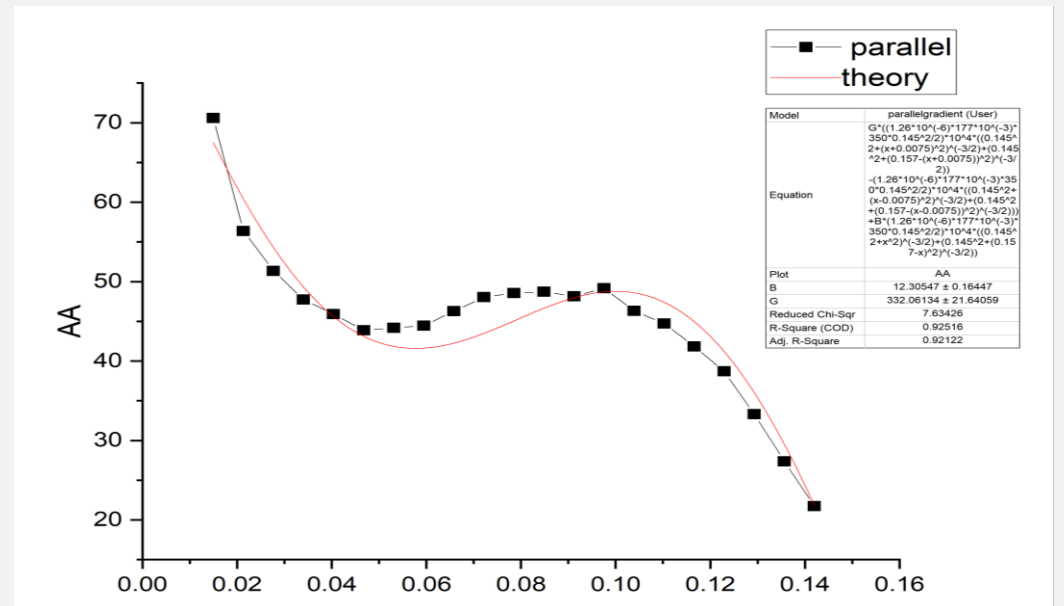
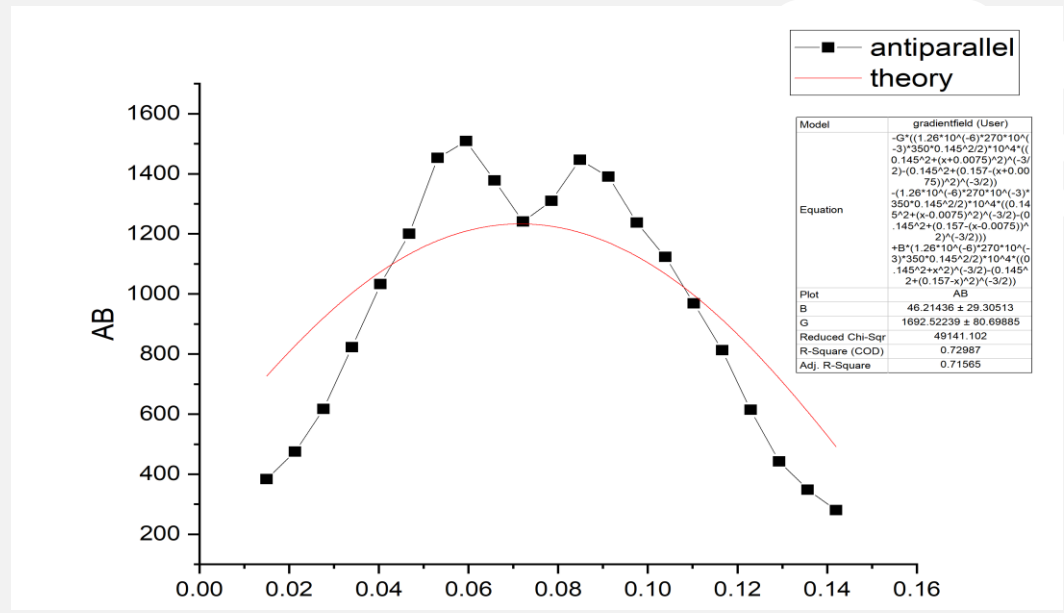
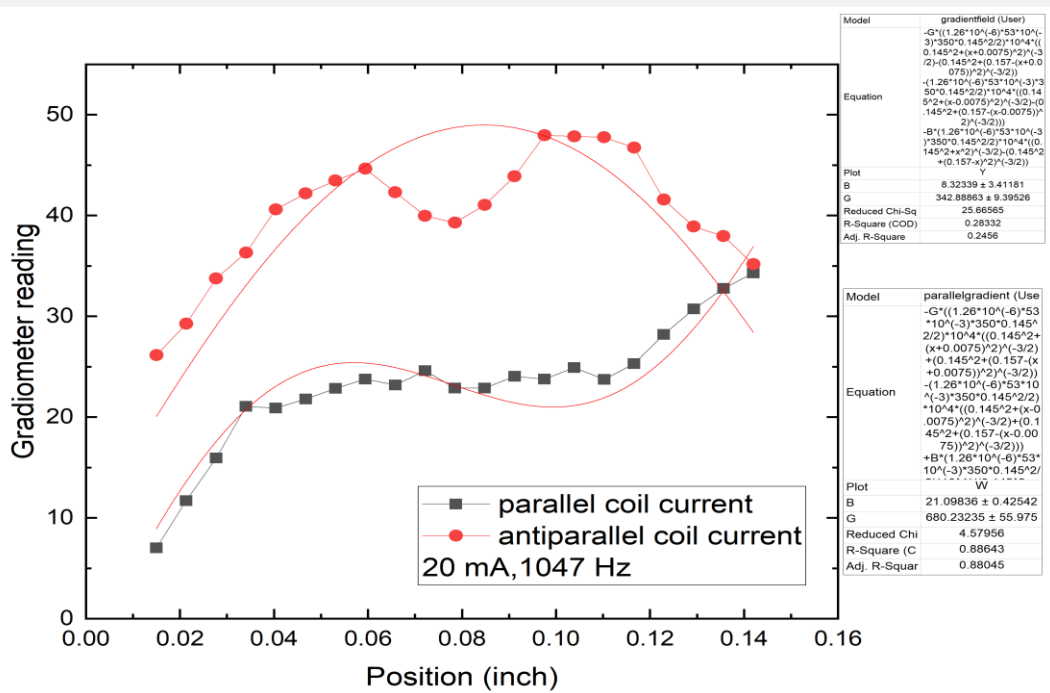


Fig. 12. Helmholtz coil calibration attempts

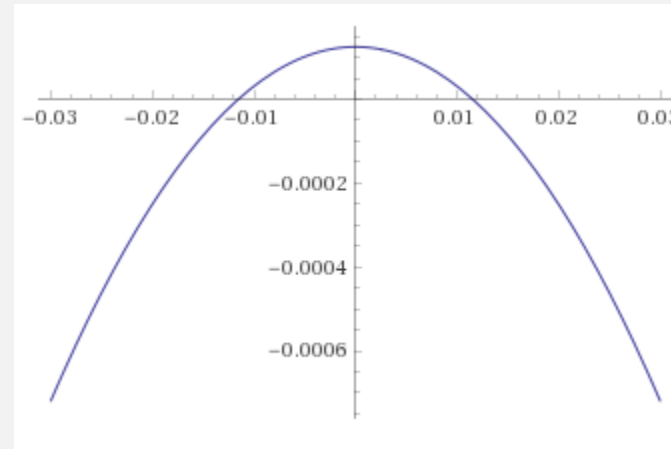
Field of the coil

The coil used currently:

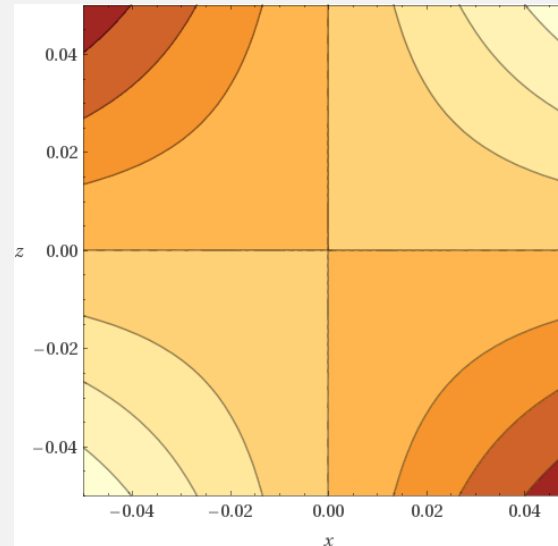
200 turns, radius 2 cm, AWG 21 (allows current up to 1.2 A)

Maximum magnetic moment 0.3 A·m² (DC field up to 55+ G)

KEPCO power supply can be very useful for getting large DC current, but does not give out large AC current when connected to the signal generator; we've used small audio amplifier instead and a box of capacitors to reach the resonance (the inductance of small coil is around 3 mH)



$$H_z = \frac{M_z}{4\pi R^3} \left(1 - \frac{3z^2}{R^2} \right) (1 + kR) + \left(1 - \frac{z^2}{R^2} \right) k^2 R^2 e^{-kR}$$

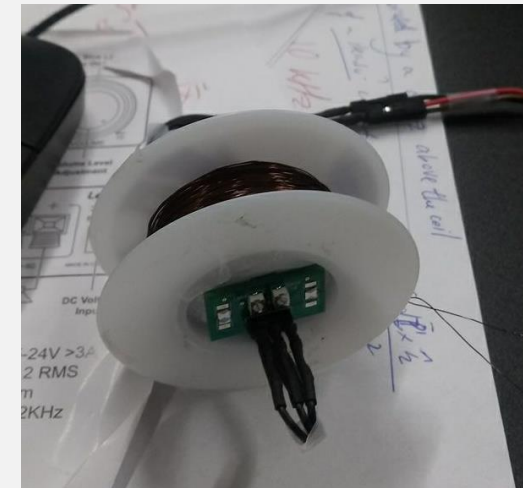


$$H_x = \frac{M_z x z}{4\pi R^5} (3 + 3kR + k^2 R^2) e^{-kR}$$

Fig. 13. Field of the small coil



$$k^2 = -i\omega\mu\sigma - \omega^2\mu\sigma$$



Attempts to detect a hole

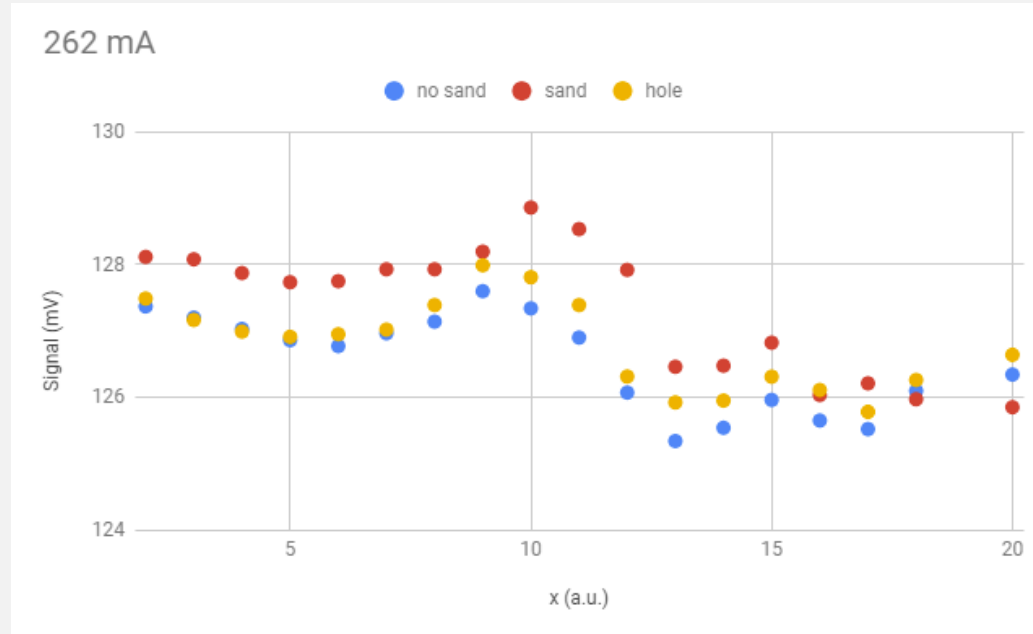


Fig. 14. First measurements

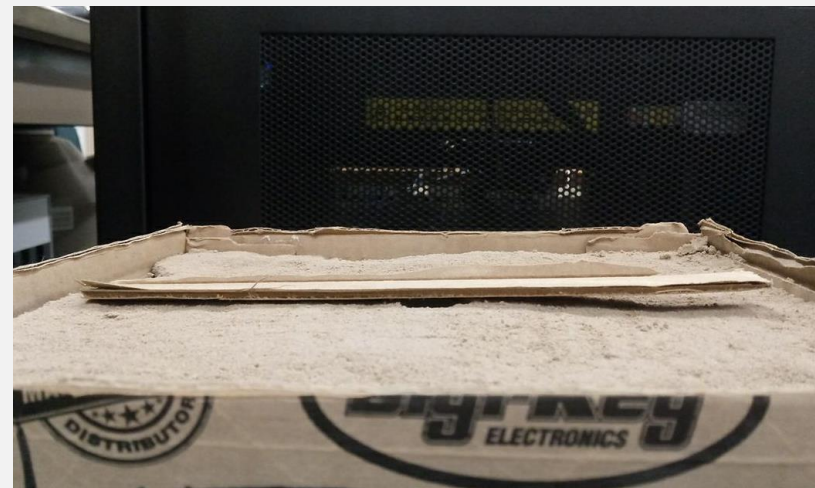
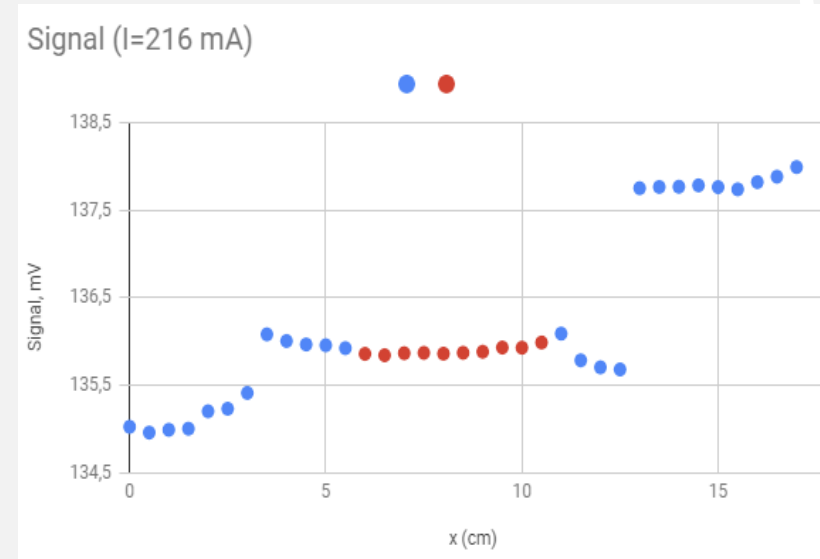
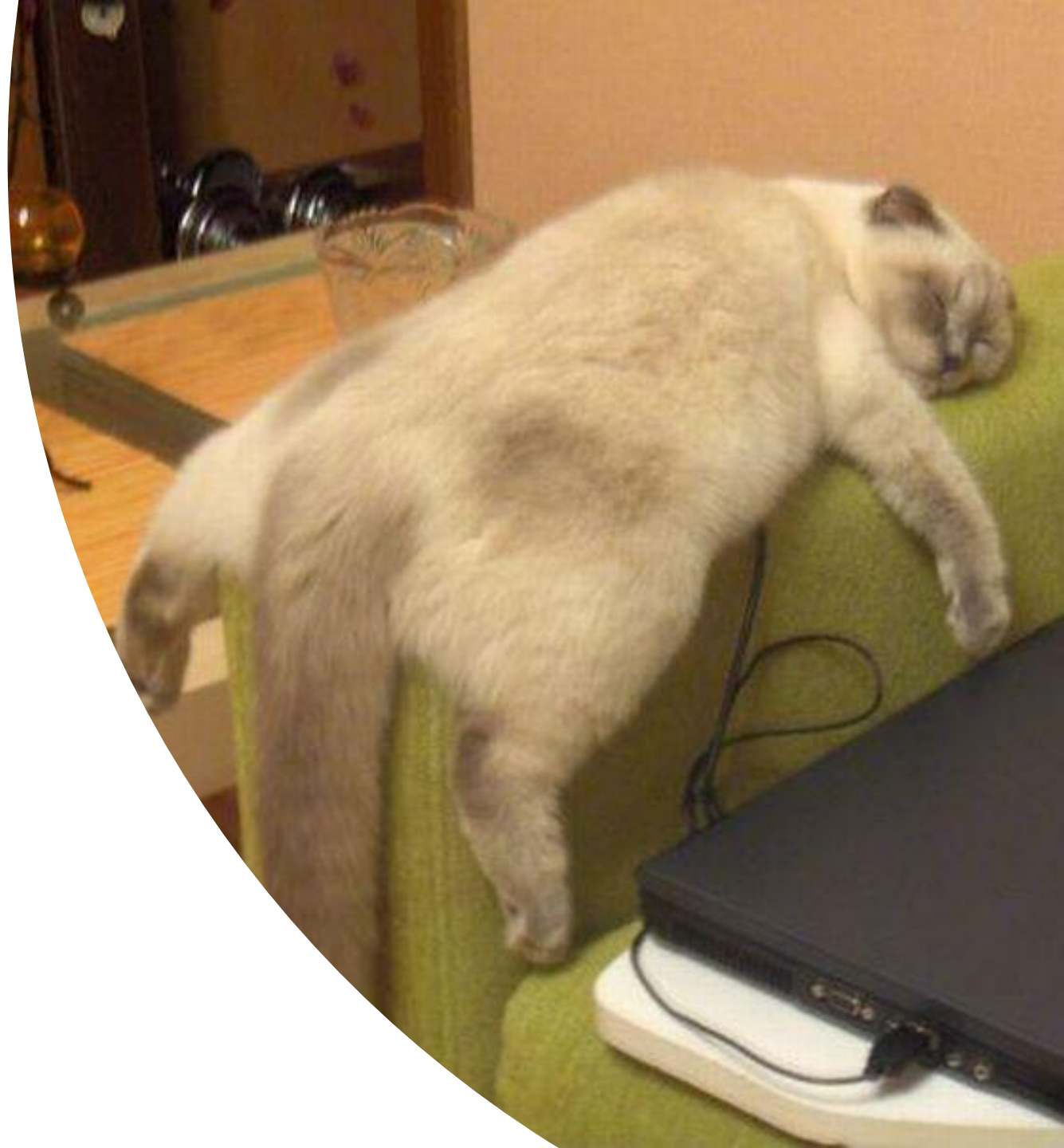


Fig. 15. Second measurement

Directions for the future work

- Get consistent reading
- Observe the signal from the coil (expand the field range of MTJ)
- Optimize the iron powder and magnetic sand parameters
- Optimize the choice of the coil winding and power consumption
- Push the detectability limit (currently the hole diameter is around 1 cm)
- Perform 3D simulation
- Move to the cylindrical model



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Thank you!

References

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- “PicoTesla Magnetic Sensors based on Magnetic Tunneling Junctions with Double-staged Flux Concentrators”, G. He, Y. Zhang, L. Qian, G. Xiao, - APS Meeting Abstracts, 2019

